

Table 1: Gaussian quadrature locations.

FE order	Points on $[-1, 1]$	Points on $[0, 1]$
1	$\pm \frac{1}{\sqrt{3}}$	$\frac{1}{3 + \sqrt{3}}$ $1 - \frac{1}{3 + \sqrt{3}}$
2	0 $\pm \sqrt{\frac{3}{5}}$	$\frac{1}{5 + \sqrt{15}}$ 0.5 $1 - \frac{1}{5 + \sqrt{15}}$
3	$\pm \sqrt{\frac{3}{7} - \frac{2}{7}\sqrt{\frac{6}{5}}}$ $\pm \sqrt{\frac{3}{7} + \frac{2}{7}\sqrt{\frac{6}{5}}}$	$\frac{10 + \sqrt{30}}{35 + \sqrt{35(15 - 2\sqrt{30})}}$ $\frac{10 - \sqrt{30}}{35 + \sqrt{35(15 - 2\sqrt{30})}}$ $1 - \frac{10 + \sqrt{30}}{35 + \sqrt{35(15 - 2\sqrt{30})}}$ $1 - \frac{10 - \sqrt{30}}{35 + \sqrt{35(15 - 2\sqrt{30})}}$

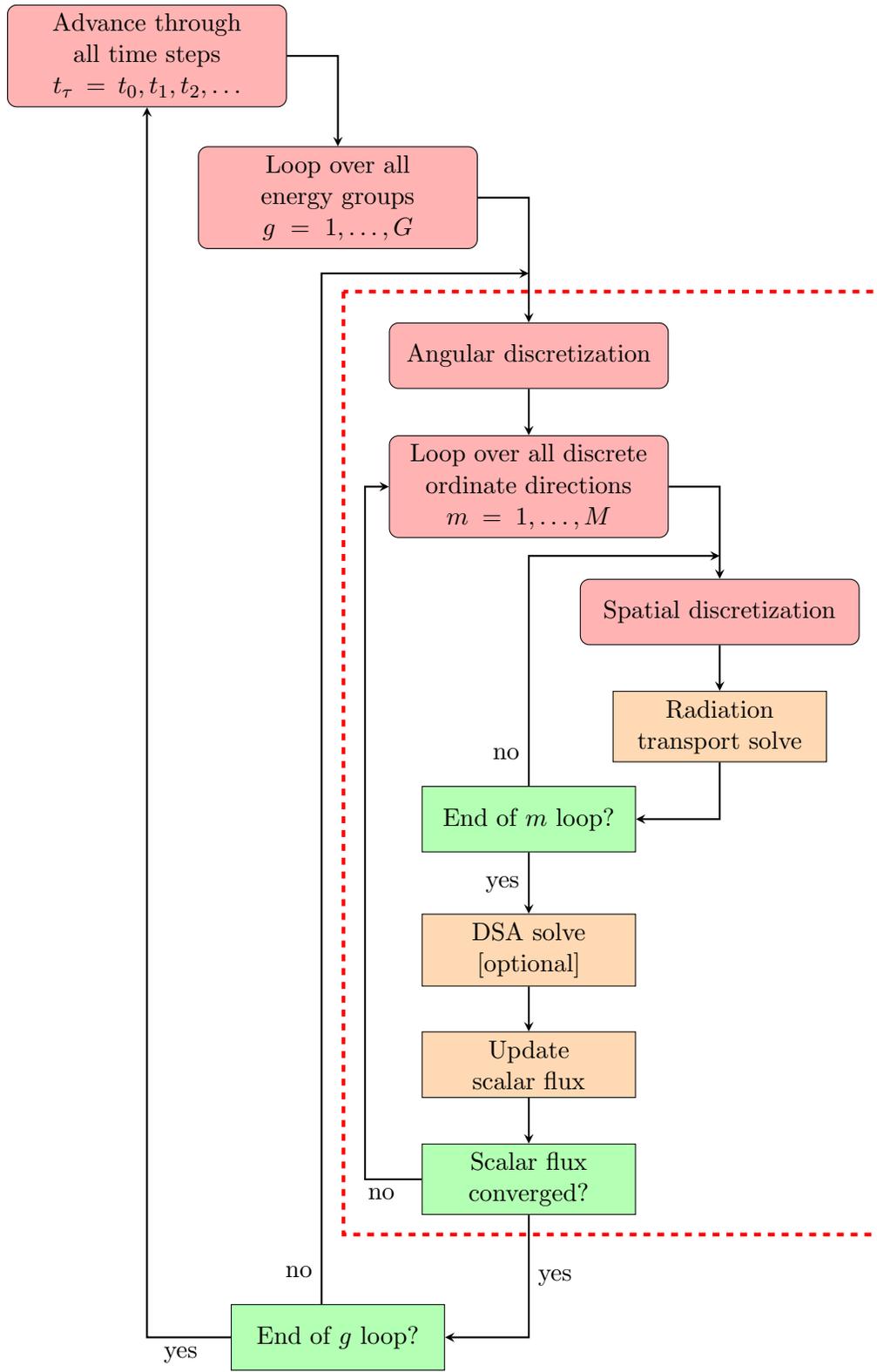


Figure 1: Flow diagram for solution process. This research is focused on the processes boxed by the dashed line.

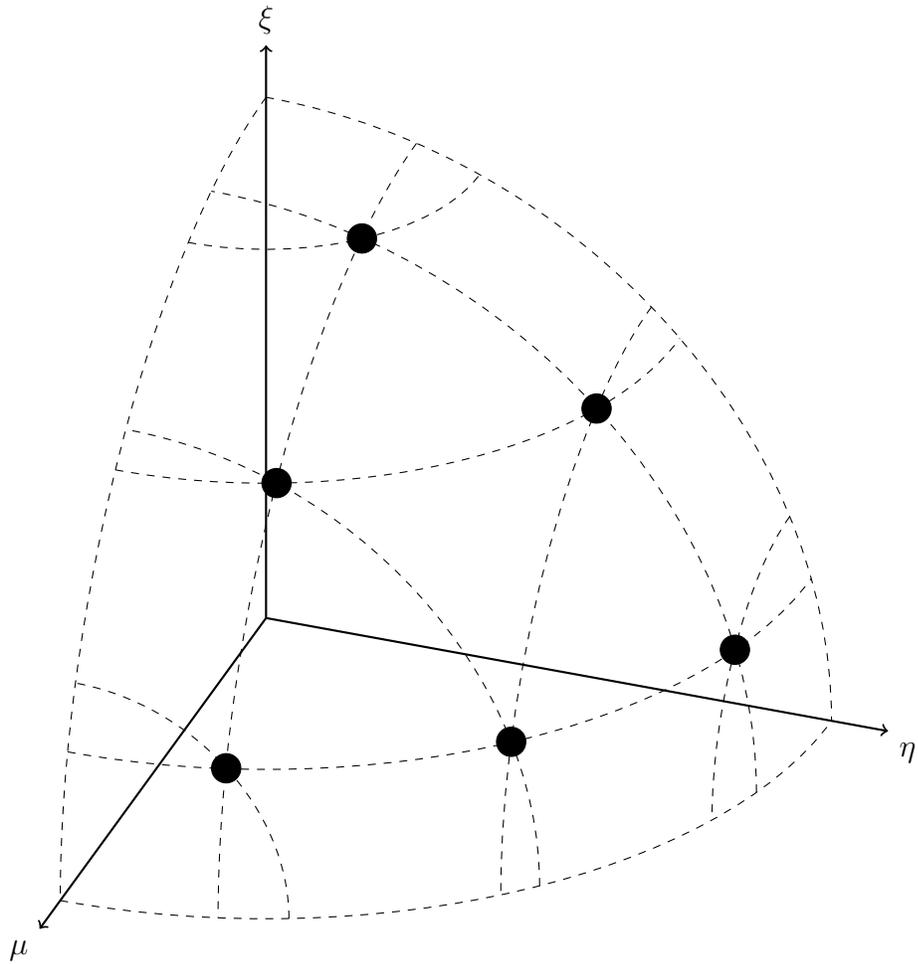


Figure 2: The positive octant for S_6 level-symmetric angular quadrature.

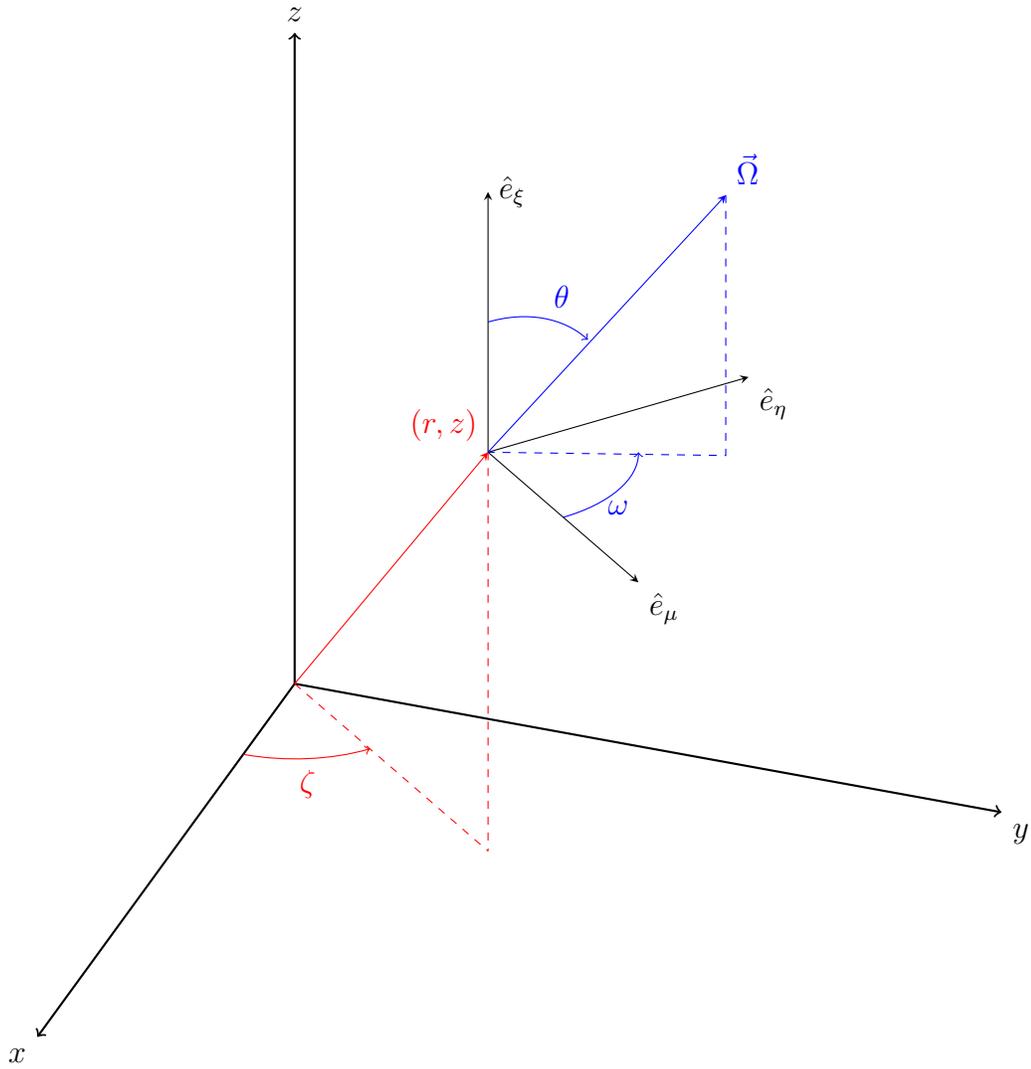


Figure 3: Cylindrical space-angle coordinate system showing the position (r, z) and direction of travel $\vec{\Omega}$.

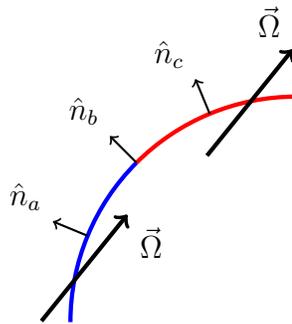


Figure 4: Example of an incident and outgoing surface.

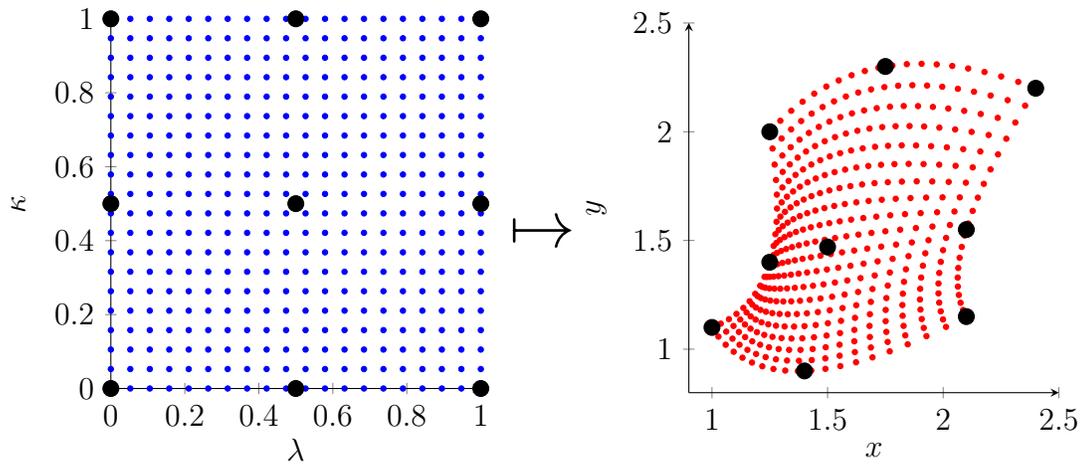


Figure 5: Example of mapping the reference element to a physical element.

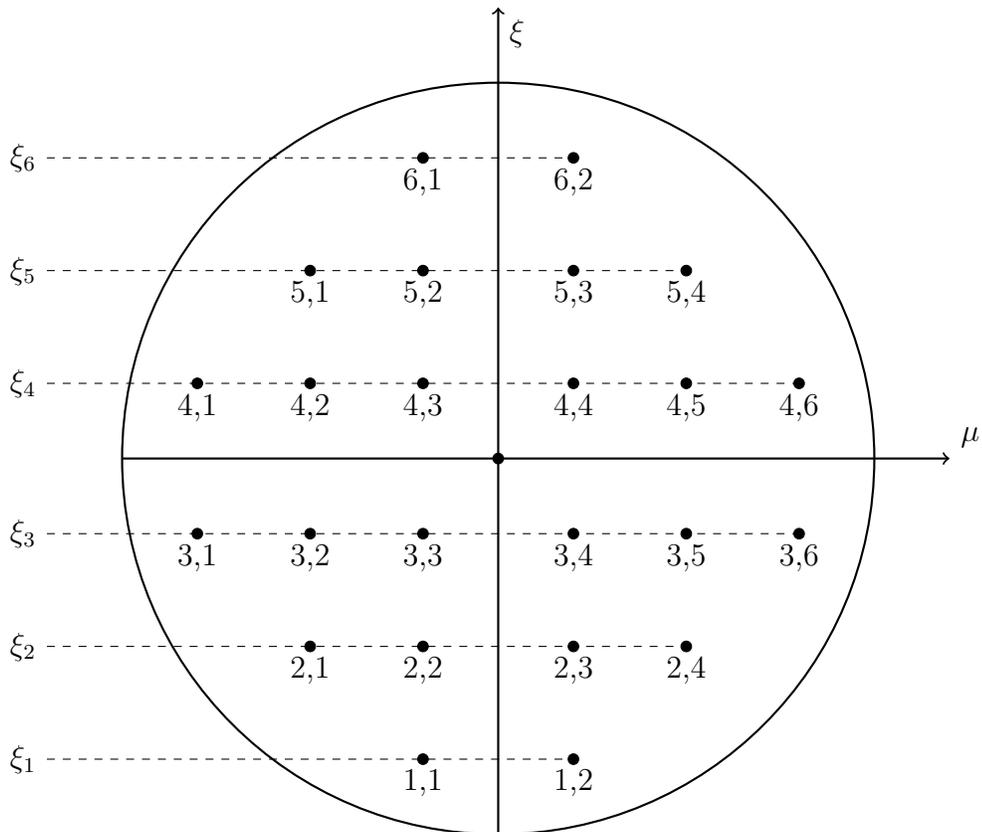


Figure 6: Angular discretization showing (ξ, μ) pairs; adapted from [?]

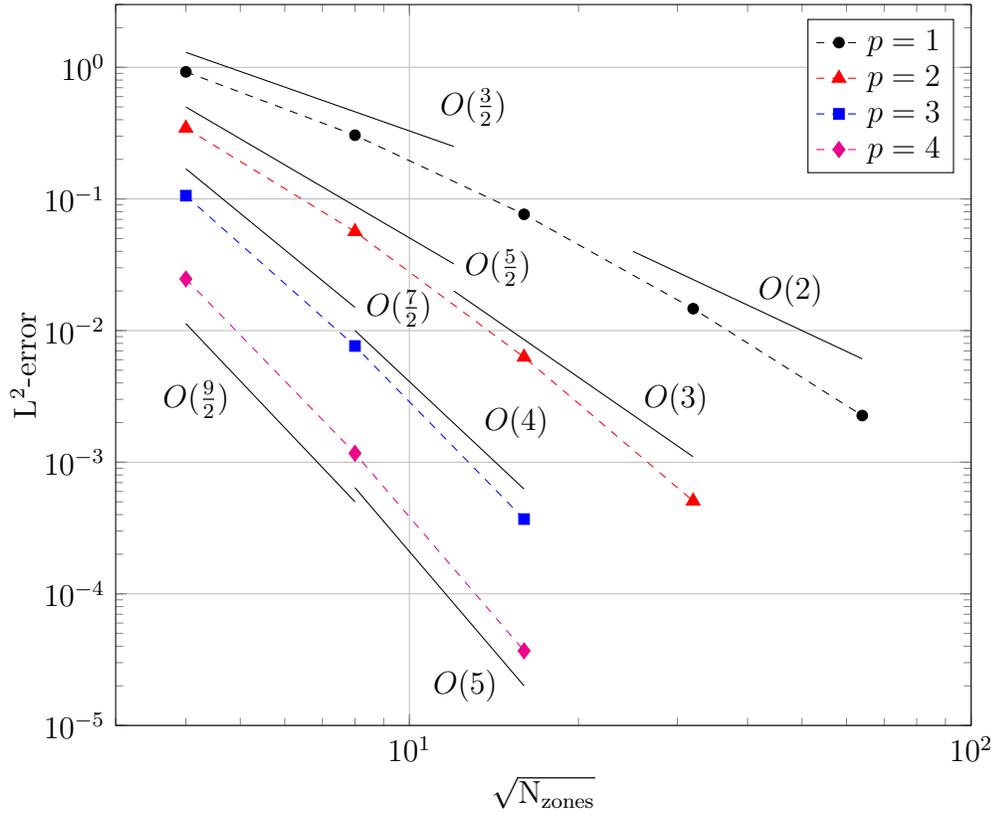
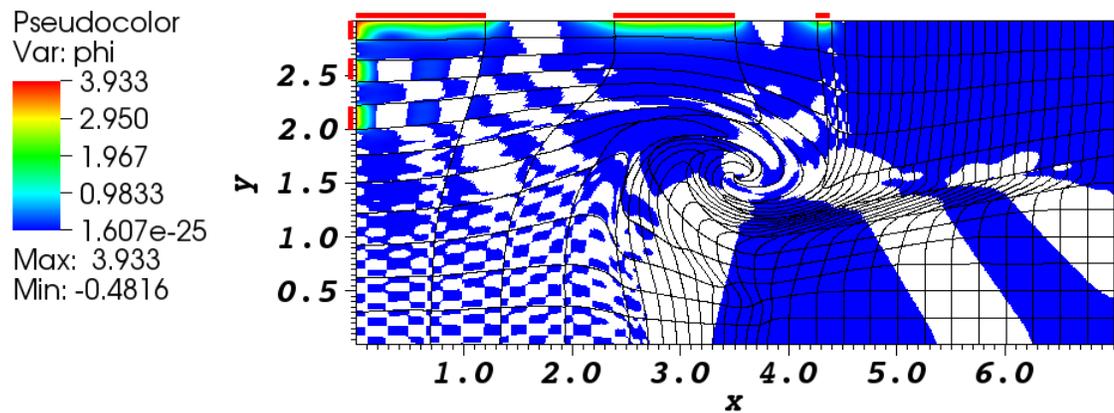
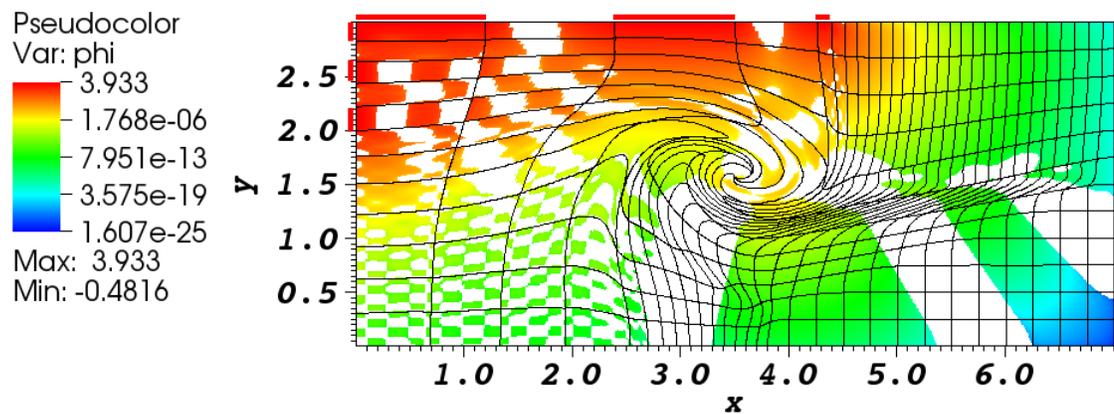


Figure 7: Errors between the manufactured and DFEM solutions. Reference lines depict order of spatial convergence $O(n) \equiv O\left((N_{\text{zones}})^{n/2}\right)$.



(a) Scalar flux; red bars denote incident boundary locations.



(b) Log of the scalar flux; red bars denote incident boundary locations.

Figure 8: Scalar flux solution for Test Problem 3.

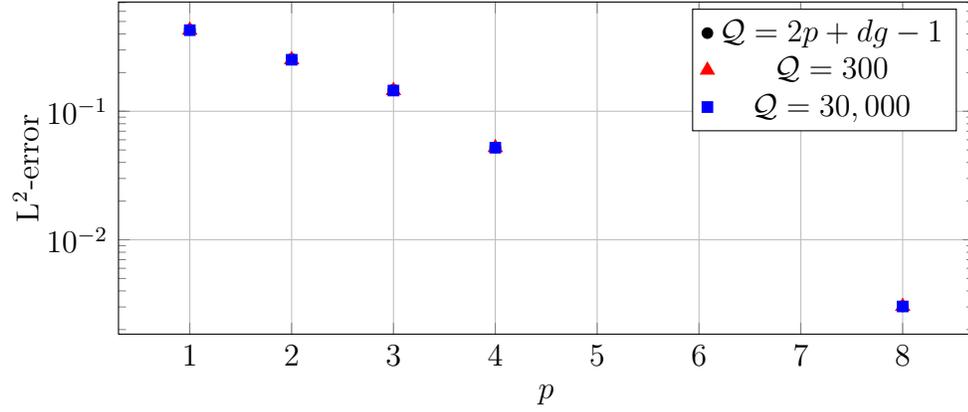


Figure 9: Error for various surface numerical integration order schemes, where p is the finite element order, g is the mesh order, and $d = 2$ is the spatial dimension of the problem.

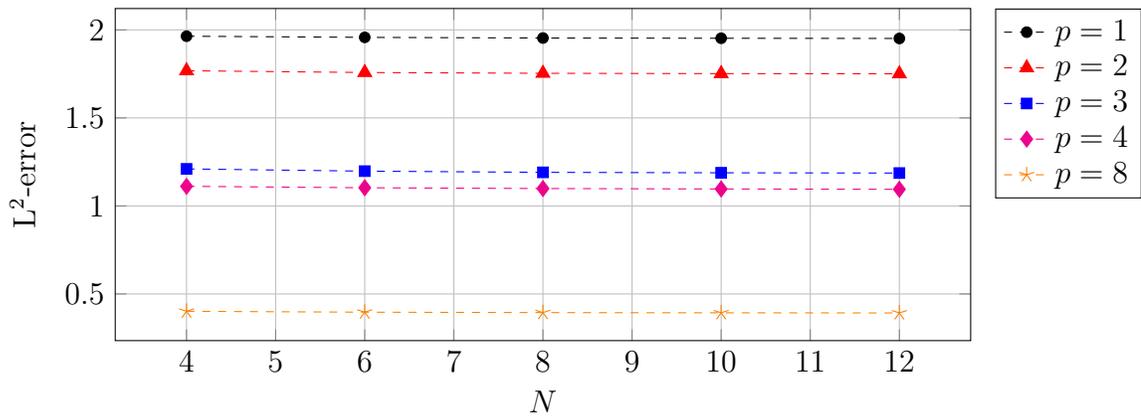
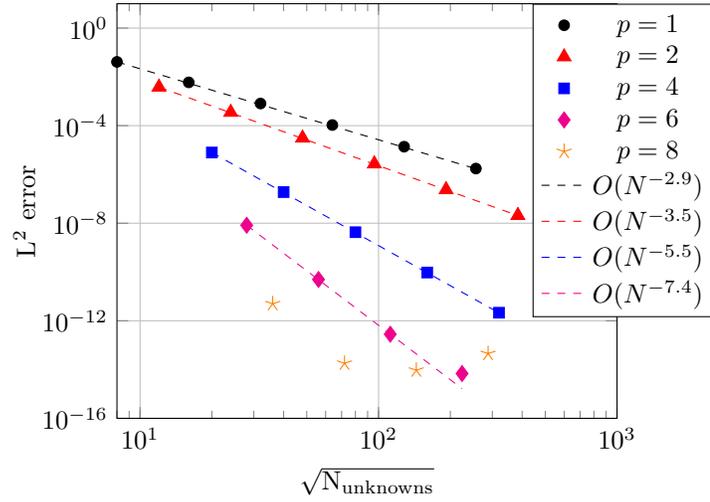
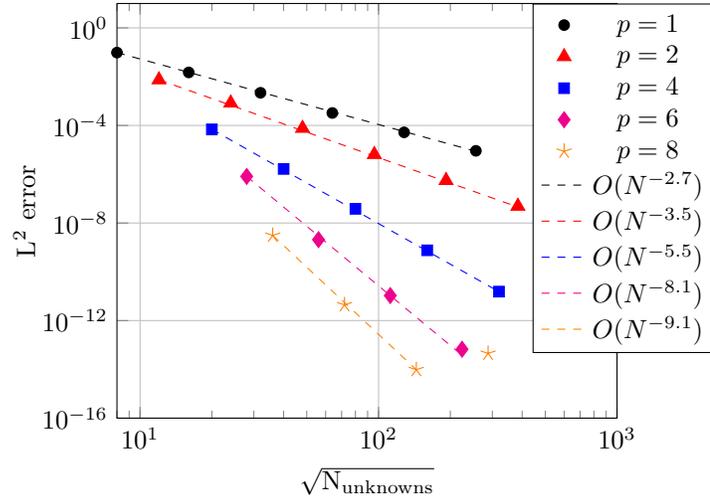


Figure 10: Error for various S_N orders.



(a) Orthogonal quadrilateral mesh.



(b) 2nd-order curved mesh.

Figure 11: L^2 -norm of the errors from the manufactured solution and reference lines computed from a least squares fit, where $N_{\text{unknowns}} = N_{\text{cells}}(p + 1)^2$.

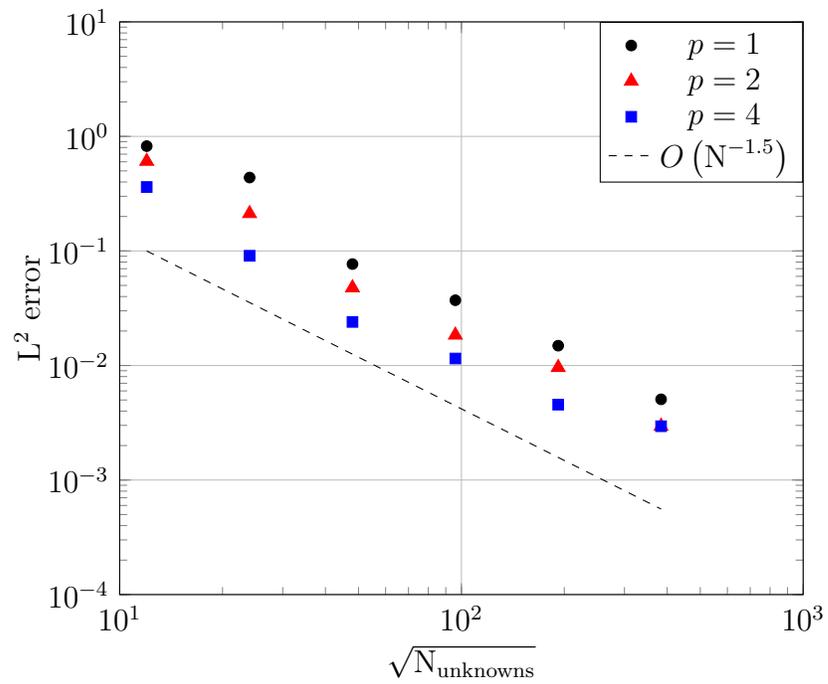


Figure 12: L^2 -norm of the errors from the manufactured solution and reference line, where $N_{\text{unknowns}} = N_{\text{cells}}(p + 1)^2$.

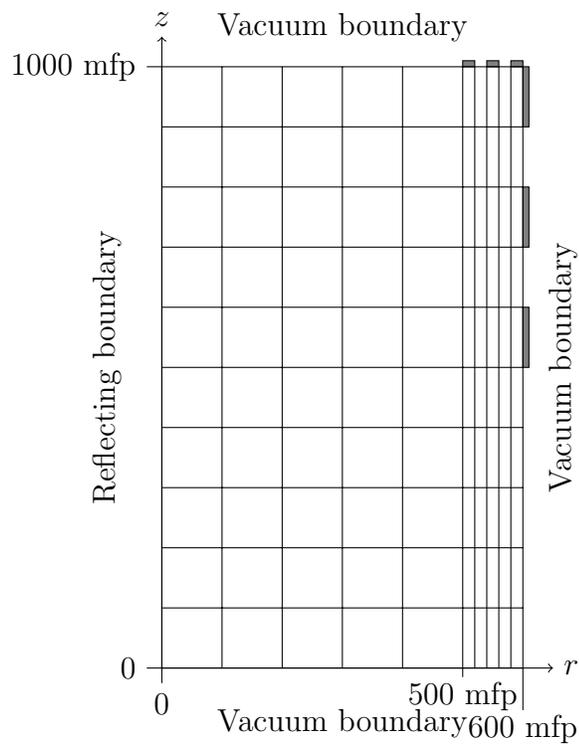


Figure 13: Strong scatter with discontinuous BCs with MIP DSA problem geometry; gray boundaries indicate incident boundary locations.

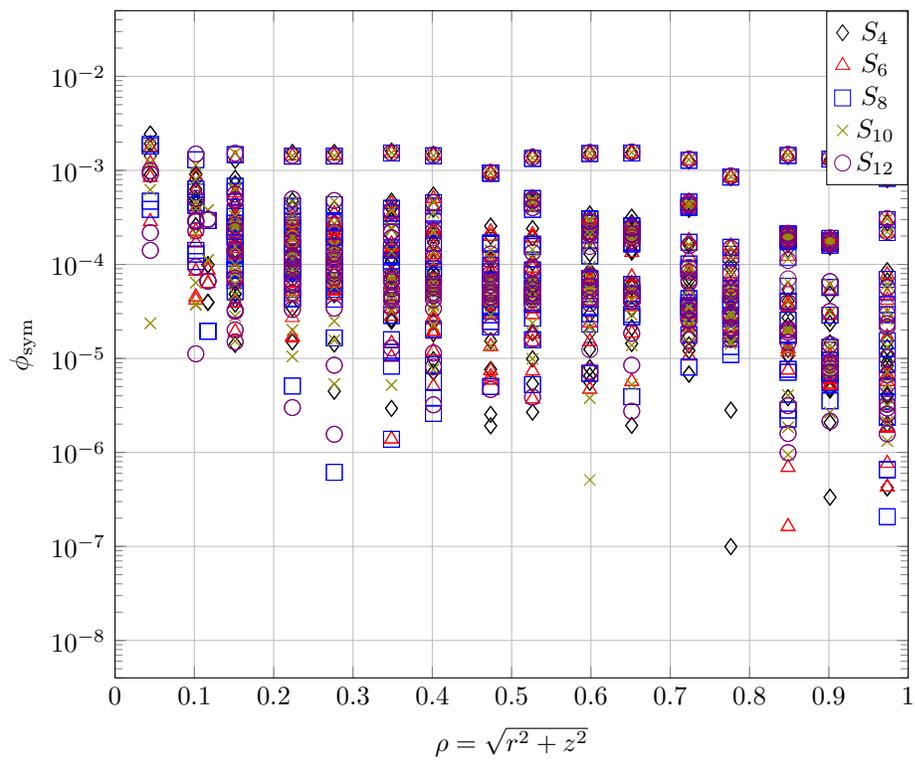


Figure 14: Measure of the asymmetry for each finite element node for the given level-symmetric angular quadrature order for 1st-order DFEM and 1st-order mesh with 120 zones (see Figure ??).

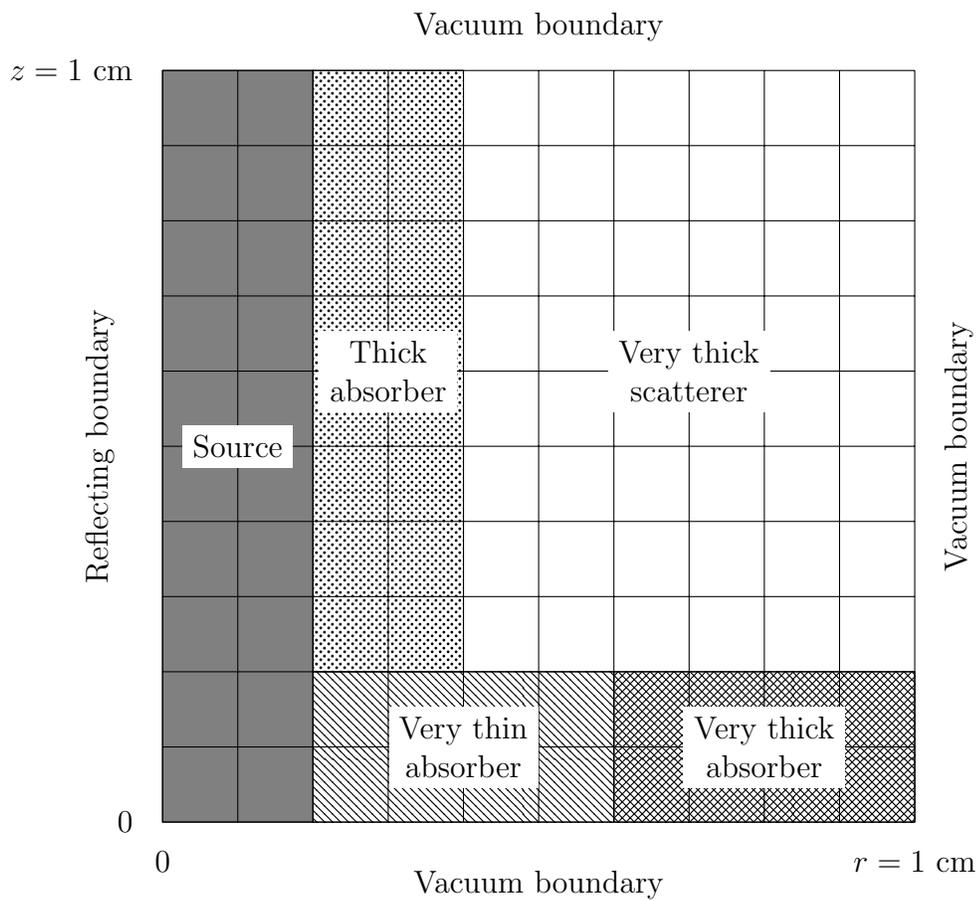


Figure 15: Material discontinuity stress test with MIP DSA problem geometry; materials defined in Table ??.

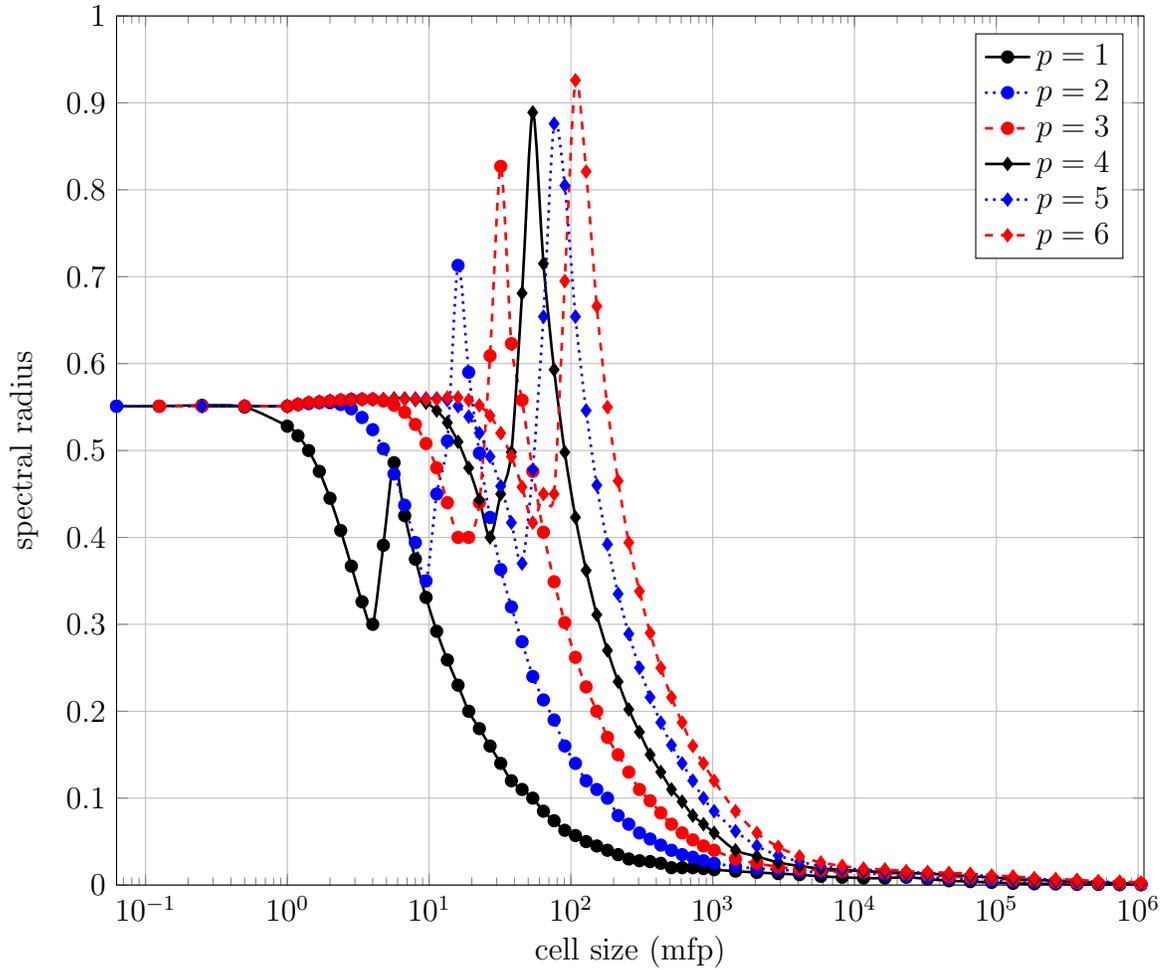


Figure 16: Spectral radius data for varying p with $C = 2$ on an orthogonal mesh with homogeneous Dirichlet boundary conditions in the DSA solve; plot reproduced from Woods et al. [?].

no.	Discretized Equation	MFEM Equation	MFEM Integrator Function
1	$(r \mu_{n,m} \cdot \partial_r \psi_{n,m,j}, v_i)_{\mathcal{D}_k}$ $(r \xi_m \cdot \partial_z \psi_{n,m,j}, v_i)_{\mathcal{D}_k}$	$(r \alpha \mathbf{\Omega} \cdot \nabla \psi, v)_{\mathcal{D}_k}$	RZConvectionIntegrator($\mathbf{\Omega}, \alpha$)
2	$(r \mu_{n,m} \cdot \hat{n} \psi_{n,m,j}, v_i)_{\mathcal{D}_k^e}$ $(r \xi_m \cdot \hat{n} \psi_{n,m,j}, v_i)_{\mathcal{D}_k^e}$	$\alpha (r \mathbf{\Omega} \cdot \hat{n} \psi, v)_{\partial \mathcal{D}_k^e}$ $+\beta (r \mathbf{\Omega} \cdot \hat{n} \psi, v)_{\partial \mathcal{D}_k^e}$	RZDGTraceIntegrator($\mathbf{\Omega}, \alpha, \beta$)
3	$(r \mu_{n,m} \cdot \hat{n} \psi_{n,m,j}, v_i)_{\mathcal{D}_k^b}$ $(r \xi_m \cdot \hat{n} \psi_{n,m,j}, v_i)_{\mathcal{D}_k^b}$	$\alpha (r \mathbf{\Omega} \cdot \hat{n} \psi, v)_{\partial \mathcal{D}_k^b}$ $+\beta (r \mathbf{\Omega} \cdot \hat{n} \psi, v)_{\partial \mathcal{D}_k^b}$	RZDGTraceIntegrator($\mathbf{\Omega}, \alpha, \beta$)
4	$(\mu_{n,m} \psi_j, v_i)_{\mathcal{D}_k}$	$(\mu_{n,m} \psi, v)_{\mathcal{D}_k}$	MassIntegrator($\mu_{n,m}$)
5	$\left(\frac{\alpha_{m+1/2^n}}{\tau_{n,m} w_{n,m}} \psi_j, v_i \right)_{\mathcal{D}_k}$	$\left(\frac{\alpha_{m+1/2^n}}{\tau_{n,m} w_{n,m}} \psi, v \right)_{\mathcal{D}_k}$	MassIntegrator($\frac{\alpha_{m+1/2^n}}{\tau_{n,m} w_{n,m}}$)
6	$(r \sigma_t \psi_j, v_i)_{\mathcal{D}_k}$	$(r \sigma_t \psi, v)_{\mathcal{D}_k}$	RZMassIntegrator(σ_t)
7	$\frac{1}{4\pi} (r \sigma_s \phi, v_i)_{\mathcal{D}_k}$	$(r \varphi, v)_{\mathcal{D}_k}$	RZDomainLFIntegrator($\frac{1}{4\pi} \sigma_s \phi$)
8	$\frac{1}{4\pi} (r S_0, v_i)_{\mathcal{D}_k}$	$(r S_0, v)_{\mathcal{D}_k}$	RZDomainLFIntegrator($\frac{S_0}{4\pi}$)
9	$(r \mathbf{\Omega} \cdot \hat{n} \psi_{inc}, v_i)_{\partial \mathcal{D}_k}$	$\frac{\alpha}{2} (r \psi_{inc} \mathbf{\Omega} \cdot \hat{n}, v)_{\partial \mathcal{D}_k}$ $-\beta (r \psi_{inc} \mathbf{\Omega} \cdot \hat{n} , v)_{\partial \mathcal{D}_k}$	RZBoundaryFlowIntegrator($\psi_{inc}, \mathbf{\Omega}, \alpha, \beta$)

Table 2: MFEM R-Z transport operator function calls where the arguments have been dropped.